

# MECA Electrometer: Overview

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## ABSTRACT

The Mars '01 lander contains an electrometer designed to evaluate the electrostatic nature of the Martian regolith and atmosphere. The objective is to gain a better understanding of the hazards related to the human exploration of Mars. The instrument has four sensor types: (a) triboelectric field, (b) electric-field, (c) ion current, (d) temperature. Only the triboelectric sensors are described in this paper

**INTRODUCTION:** The electrometer is part of MECA (Mars Environmental Compatibility Assessment) project. It will be built into the heel of the Mars '01 robot arm scoop as seen in Fig. 1. The robot arm is two-meters in length; thus, the electrometer must operate over an 8-wire serial interface. It will be housed in a volume of  $\sim 50 \text{ cm}^3$  and consume 150 mW.

The triboelectric field sensor array consists of five insulating materials to determine material charging effects as the scoop is dragged through the Martian regolith. These materials will be chosen after Earth-based tests using Mars simulant soils.

**OPERATION:** In operation the triboelectric sensors will be rubbed against the Martian soil as depicted in Fig. 2. After reaching the end of its traverse, the scoop will be abruptly removed from the soil at which time the triboelectric sensor response will be measured. The parameters for this operation are shown in Fig. 2 and typical values are listed in the figure caption.

**DESIGN:** The design of the triboelectric sensors follows from the traditional electrometer as depicted in Fig. 3. Here the electrometer has three capacitors, C1, C2, and C3 where C1 is connected to an operational amplifier that is operated in the follower mode. In the

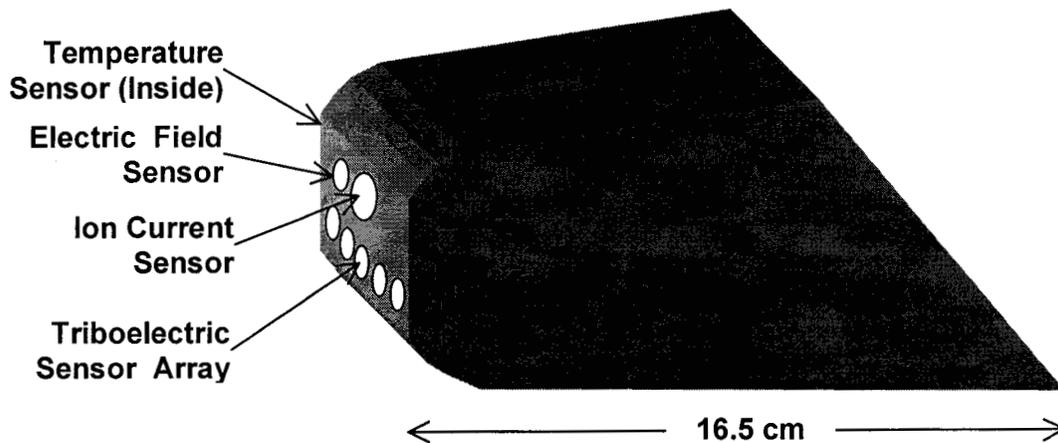


Figure 1. Electrometer sensor suite mounted in the heel of the Mars '01 scoop.

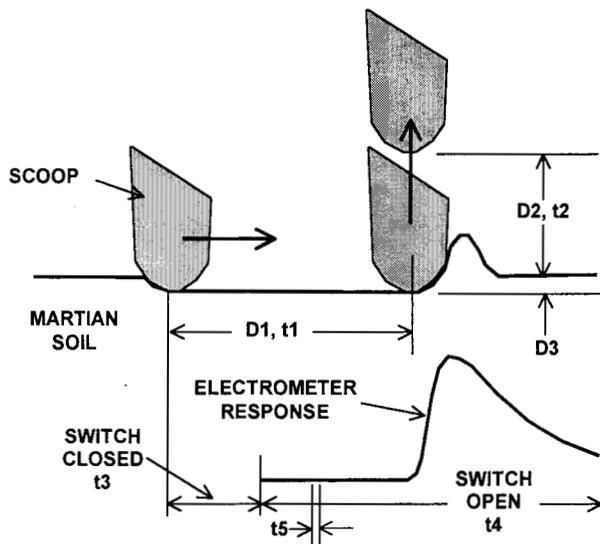


Figure 2. Operational scenario for the scoop where recommended operating parameters are:  $D1 = 10$  cm,  $D2 = 1$  cm,  $D3 = 0.5$  to  $1$  cm,  $t1 = 10$  s,  $t2 = 0.5$  s,  $t3 = 1$  s,  $t4 = 19$  s,  $t5 = 0.1$  s

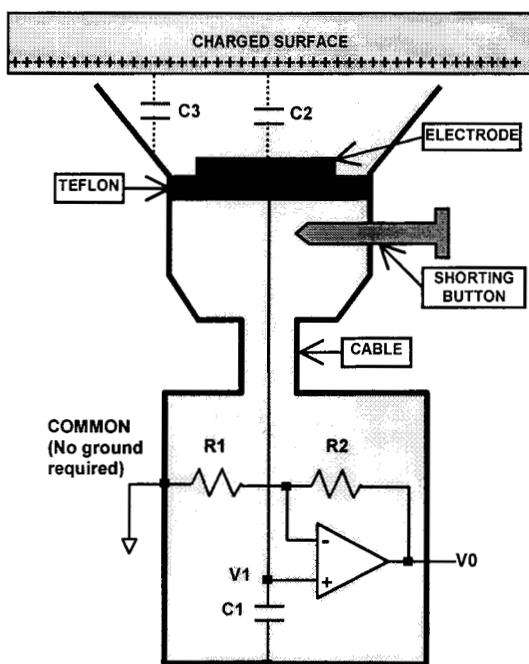


Figure 3. Traditional electrometer [1] typically used to measure ESD, electrostatic discharge, in a laboratory setting.

triboelectric sensor developed here, the mechanical switch has been replaced by a low-leakage solid-state switch and is used to remove the charge from  $C1$ . In addition  $C2$  was replaced by an insulator that will be rubbed against the Martian soil so as to determine the

potential for build up of charge on various insulating materials.

MODEL: An electric circuit model, shown in Fig. 4, was developed to aid in the design and analysis of the sensor. The model includes the previously described capacitors and switch. It also includes a resistor that represents the discharge mechanism for the insulator,  $C2$ .

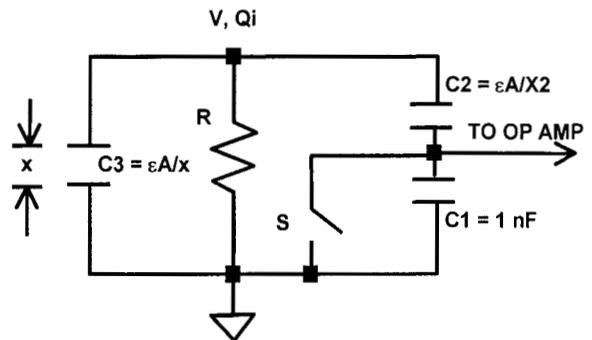


Figure 4. RC circuit model for the triboelectric sensors.

The model assumes that the triboelectric sensor, after rubbing the surface, lifts off from the surface with a constant velocity,  $v$ , and a charge  $Q_i$ . The time from liftoff is  $t$  and the parameters are:  $\tau = R \cdot C_0$ , and  $T = \epsilon A / (v \cdot C_0)$  where  $C_0 = C_1 \cdot C_2 / (C_1 + C_2)$  and  $C_3 = \epsilon A / X$ , where  $A$  is effective area. Thus this model contains three critical parameters:  $Q_i$ ,  $\tau$ , and  $T$ .

The response curves shown in Fig. 5 illustrate how these parameter intermingle. For  $\tau$  very large which occurs in a leak free insulator, the response curves approach  $Q_i$ . For a small  $\tau$ , the curves peak and decay rapidly. This response is the behavior that needs to be measured on Mars and is depicted in Fig. 2 along with the motion of the scoop.

EXPERIMENTS: Five different insulators were loaded into the triboelectric sensor head and were manually rubbed at room temperature with wool felt and the results are shown in Fig. 6. The response around 0.2 minutes is during the rubbing process. After secession of rubbing the curves show a small loss of charge which indicates that all these insulators have good

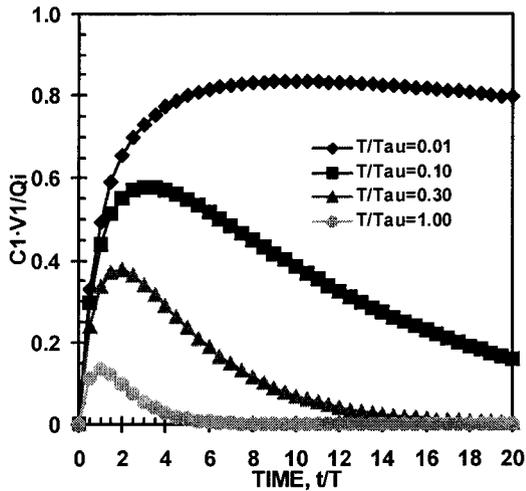


Figure 5. Time response predicted for the triboelectric sensors using the RC-circuit model shown in Fig. 4.

insulating properties. In addition, the response shows both positive, zero, and negative behavior. The zero behavior may have identified an important antistatic material. The voltage response at the output of the amplifier had a gain of four with respect to the input.

Subsequent rubbings revealed similar response but differed in magnitude due to the relatively uncontrolled nature of the rubbing process. That is the velocity, pressure, and time of rubbing were not well controlled in this initial experiment.

**MARS EXPERIMENTS:** The five materials that can be triboelectrically rubbed on Mars must be chosen carefully. The materials will be chosen to span the electrostatic parameter space given by  $Q_i$ ,  $T$ , and  $\tau$ . Next Earth-bound tests will be developed to characterize candidate materials in simulated Martian soils. From these test results, the five triboelectric flight will be chosen.

**DISCUSSION:** A new triboelectric sensor instrument has been developed. It is about to under go extensive ground testing from which the five materials will be chosen. These materials will be flown to Mars and tested.

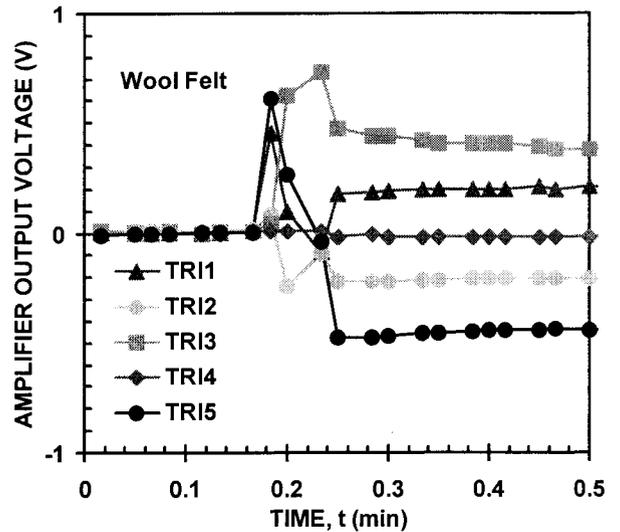


Figure 6. Experimental response curves from five triboelectric sensors where TRI1 is ABS, TRI2 is polycarbonate, TRI3 is linen filled phenolic, TRI4 is Rulon-J, and TRI5 is Teflon which were rubbed with wool felt.

These results will be compared to Earth-bound tests. If the tests agree then new Mars bound materials can be evaluated with confidence. If significant discrepancies arise between the Earth and Mars tests, then one must proceed more cautiously and re-evaluate our understanding of how triboelectrically materials respond to the Martian environment.

**REFERENCE:**

1. Electrometer Measurements, Keithley Instruments, 1972

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